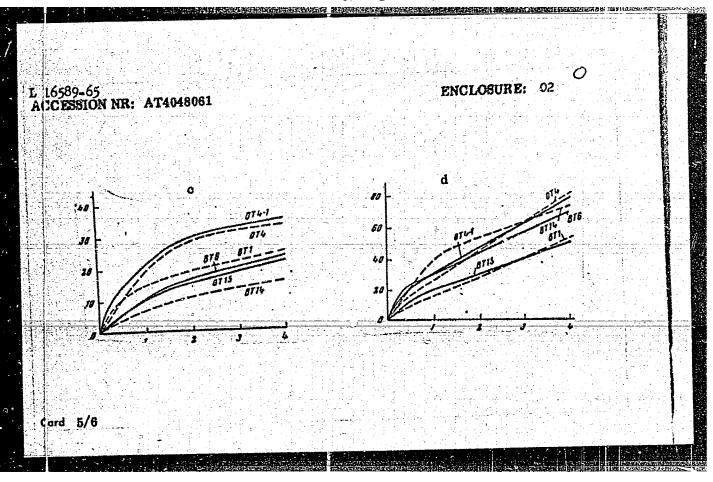
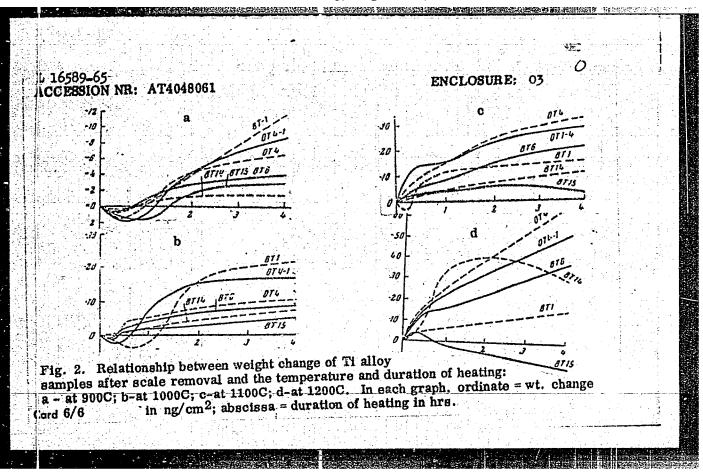


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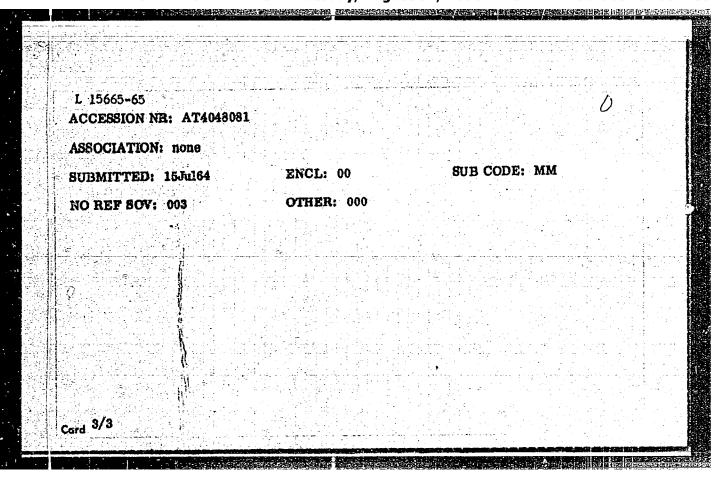


L 15665-65 ENT(m)/ENP(w)/EWA(d)/EWP(t)/EWP(k)/EWP(b) Pf-4 ASD-3/AFFTC/ ESB-3/IJP(c)/ASD(f)-2/ASD(m)-3 MJW/JD/HW/MLK ACCESSION NR: AT4048081 S/0000/64/000/000/0249/0254 8/0000/64/000/000/0249/0254 AUTHOR: Pavlov, I.M., Tarasevich, Yu. F., Shelest, A. Ye. TITLE: Effect of the conditions of plastic deformation and further working on the properties of several titanium alloys SOURCE: Soveshchaniye po metallurgii, metallovedeniyu i primeneniyu titana i yego splavov. 5th, Moscow, 1963. Metallovedeniye titana (Metallography of titanium); trudy\* soveshchaniya, Moscow, Izd-vo Nauka, 1964, 249-254 TOPIC TAGS: titanium alloy, titanium alloy working, plastic deformation, cooling rate, titanium alloy strength, titanium alloy hardness, titanium alloy rolling/alloy OT4. alloy VT6. alloy VT14 ABSTRACT: The authors investigated the effect of plastic deformation and subsequent cooling at different rates on the mechanical properties of several  $\sim +\beta$  b titanium alloys (martensite, types OT4, VT6 and VT14), where the B phase may be partially set at room temperature. The alloys were rolled at a rate of 0.5 m/sec followed by cooling either in water, asbestos or air. The cooling rate as measured by thermocouples was 60-70 deg/sec in water, 4.3-5 deg/sec in asbestos and 6-6.5 deg/sec in air for the VT14 alloy. Mechanical proporties were then determined. The tests showed differences in Card 1/3

L 15665-65 ACCESSION NR: AT4048081

hardness of VT14 alloy samples cooled under different conditions. All alloys showed slight variations in hardness when cooled from 500-800C with 20% compression under the roller. Hardness was increased significantly by 40% compression and lowering of the temperature from 800C. The effect of cooling rate on strength was noticeable only at rolling temperatures above 900C. For 20% compression the ultimate strength changed smoothly as the rolling temperature varied. This was not observed for higher compression values, confirming the effect of plastic deformation on the mechanical properties of the alloy. Relative narrowing was increased with compression at all rolling temperatures and cooling rates, while the temperature relationship was constant with a minimum at 1000C and maximum at 700C. Elongation was lowered during rolling at temperatures below 800C with maximum elongation at moderate cooling rates beginning with 1100C. The data obtained make it possible to plan methods for improving the mechanical properties of titanium alloys by thermomechanical working. However, the thermal stability of the alloys after working will be low and the alloys will be used successfully only at normal temperatures. Additional research is required to find ways of employing titanium alloys at higher temperatures. "Ye. G. Konstantinov took part in the investigations." Orig. art. has: 4 figures.

Card 2/3



L 9961-65 ENT(m)/T/EWP(b) ASD(m)-3 JD/MLK 5/0000/64/000/000/0336/0341	
ACCESSION NR: AT4046865 5/0000/64/000/000/0336/0341 AUTHOR: Paylov. I.M. (Corresponding member AN SSSR); Rastegayev, M.V.; Danil'chenko, A.N.; Zharov, V.M.; Falaleyeva, Z.S.; Memis, V.Ya.; Daugutov, M.Ya.	B
Vinogradov, Iu.  TITLE: Effect of primary thermoplastic treatment on the properties of a heat resistant alloy 6	
SOURCE: AN SSSR. Nauchnyky sovet po probleme zharoprochnykh splavov. Issledo vaniya starey i splavov (Studies on steels and alloys). Moscow, Izd-vo Nauka, 1964, 336-341	
TOPIC TAGS: thermoplastic treatment, heat resistant steel, steel upsetting, st microsection, heat resistant alloy, strain hardening, impact toughness, stress rupture strength	eel j
ABSTRACT: Lately, many articles have been published on plastic deformation under pressure combined with thermal treatment to obtain metals of high strength. It almost all publications, the tested metal had previously undergone treatment under almost all publications, the tested metal had previously undergone treatment under the pressure. In the opinion of the authors of the present paper, special attention should be paid to the initial thermoplastic treatment. If the required proper is the present paper and the property of the present paper is the present paper.	nder   on
are reached at this time, further treatment is unnecessary. Previously, the authors of this article investigated cast heat-resistant alloy 8 from an arc Cord 1/5	#200F0

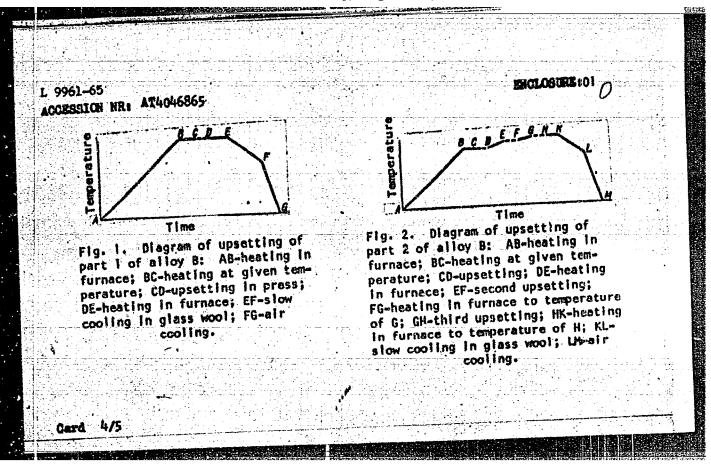
L 9961-65 ... ACCESSION NR: AT4046865 furnace by upsetting, thus obtaining various structural densities and grain boundaries affecting the heat resistance of the steel. In the given paper, heatresistant alloy B was obtained by electric slag smelting. Thus, the initial cast structure was much better than the one described in the previous paper. The B alloy is-complex and has a narrow interval for thermal treatment under pressure. The Ingot (dlam, 150 mm, length 600 mm) was cut into three equal parts of 150x200 mm. The parts were upset as shown in Figs. 1-3 of the Enclosure. The first two parts underwent the same degree of deformation, namely 0.844. The final contact coefficient (ratio of cylinder diameter to height) at the end of compression was 17.1. For the third part, the degree of deformation was 0.85 and the final contact coefficient was 12.9. Microsections showed that all three parts had a similar dense structure. Further, all three parts were cut into 20x20x70 mm samples for measurement of the yield point and strength. The third part had the highest values, while part two had the lowest. The second part had the highest impact

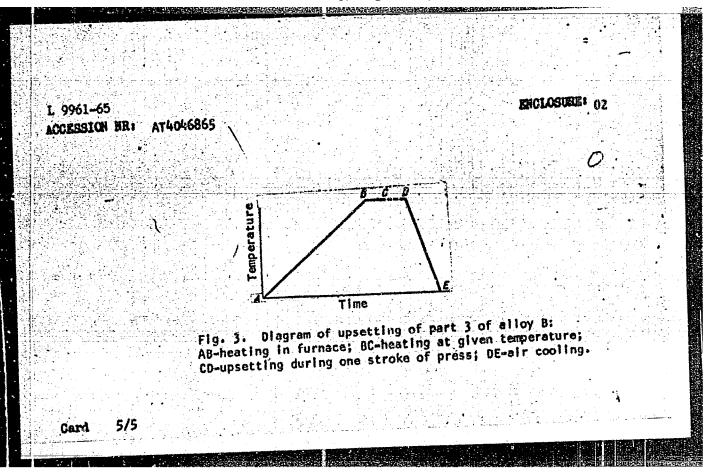
toughness, while part 3 had the lowest. The stress-rupture strength after 100 hours was 14 kg/mm<sup>2</sup> for part 1, 16 kg/mm<sup>2</sup> for part 2 and 20 kg/mm<sup>2</sup> for part 3, which

was verified by microstructural analysis; before 30 hours, the stress-rupture strength of part I was higher than that of part 2. It is noted in conclusion that thermoplastic treatment leads to high quality metals and alloys. The use of electric slag smalting improves the metal structure. Improvement of mechanical

Card 2/5

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properties depends	s to a high degree on res further investiga	the correct cho stion. Orig. art	lce of deforms. has: 5 figu	tion procedure, res, I table	
and 5 formulas.					
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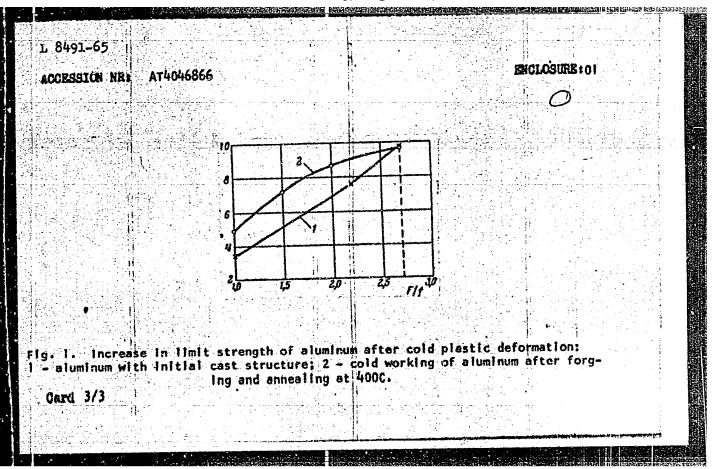




JD/HW/MI.K Pf-4/Ps-4 EWT(m)/EPR/EWP(k)/EWP(q)/EWP(b) ASD(f)5/0000/64/000/000/0342/0344 ACCESSION NR: AT4046866 AUTHOR: Pavlov, I. H. (Corresponding member AN SSSR); Zharov, V. M. TITLE: A specific case of the investigation of strain hardening of metals SOURCE: AN SSSR. Nauchnyky sovet po probleme zharoprochnykh splavov. Issledovaniya staley i splasov (Studies on steels and alloys). Moscow, Izd-vo Nauka. TOPIC TAGS: metal hardening, metal strain hardening, metal cold working, plastic deformation, aluminum, cast aluminum ABSTRACT: Metals may be hardened in different ways, including heat treatment, neutron bombardment, cold working, etc., but hardening by cold plastic deformation has not been investigated sufficiently. Usually, cold working is employed with metals which have previously been subjected to thermal pressure treatment. However, the present development of continuous metali casting suggests that cast ingots will soon be used for cold stamping. The present paper therefore compares strain hardening of cast metal with metal hardening by pressure with recrystallization during annealing. The cast aluminum tested had only 0.02% of inclusions and a limit strength of 3.5 kg/mm2. Two other cast billets cut from the ingot were drawn cut on the MP-75 pneumatic hammer and cooled in water after each impact.

# L 8491-65 ACCESSION NR: AT4046866 of deformation is usually estimated by the "forging coefficient" which shows the ratio between the billet cross section before and after drawing, or the ratio of Initial and final lengths. Fig. I of the Enclosure shows the Increase in limit strength of aluminum after cold plastic deformation. The second part of the investigation considered the strength after cold working of the same aluminum previously heat treated under pressure and annealed. The limit strength of the annealed aluminum was 4.9 kg/mm2. Fig. 1 shows that at y=2.72 maximal/hardening is reached. Comparison of cold working of cast and hot-forged metal shows that the cast metal, after cold working, reaches the strength of forged metal which had a higher initial strength. It is found that cast aluminum billets may also be used for cold working. The strain hardening of cast aluminum is more rapidly effective than the cold working of aluminum previously hardened under pressure and recrystallized. Cold working of cast metal gives the same results as hot-treated metal when the actual deformation equals 2.72. Orig. art. has: 2 figures. ASSOCIATION: none SUB CODE: ENCL: 01 SUBMITTED: 16Jun64 OTHER: NO REF SOVE 000 Card 2/3

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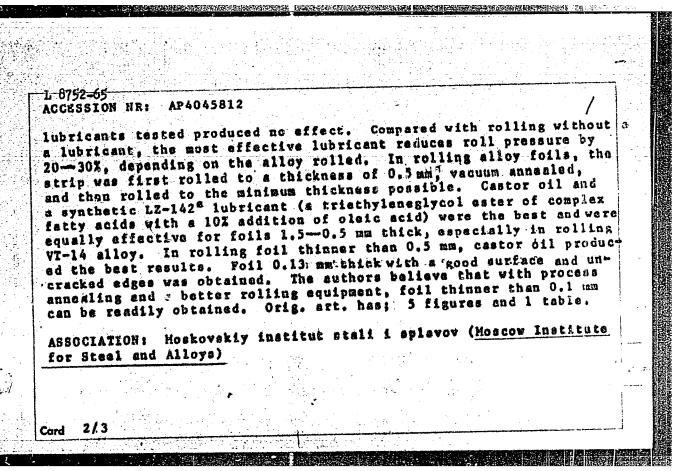
PAVLOV, I.M.; OSADCHIY, V.Ya.; GETIYA, I.G.; FROLOCHKIN, V.V.;
KOLIKOV, A.P.

Investigating the process of rapid cross rolling. Izv. vys.
ucheb. zav.; chern. met. 7 no.3:107-112 '64. (MIRA 17:4)

1. Moskovskiy institut stali i splavov.

是一个企业的企业的国际企业的基础的。 1987年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1988年—1

L 8752-65 EWI(m)/KPF(c)/T/EWP(k)/EWP(b) Pf- $\frac{1}{2}$ /Pr- $\frac{1}{2}$  IJP(c)/ASD(m)-3 HW/DJ 5/0145/64/000/009/0088/0094 ACCESSION NR: AP4045812 AUTHOR: Pavlov, I. H.; Burkhanov, S. F.; Shor, E. R.; Osipov, E. Ye. Chinenov, A. H. TITLE: Effect of lubricants on cold rolling of thin strips and foil from VI-14 VI-15 and VI-16 titanium alloys SOURCE: IVUZ. Chernaya metallurgiya, no. 9, 1964, 88-94 TOPIC TAGS: titanium alloy, VT-14 alloy, VT 15 alloy, VT 16 alloy, alloy cold rolling, strip rolling, foil rolling, lubrication effect ABSTRACT: Titanium-base VT-14, VT-15, and VT-16 alloys with a tensile strength and elongation (in the aged condition) ranging from 115 to 160 kg/mm 2 and from 3 to 10%, respectively, were rolled to an initial thickness of 1.5 mm, vacuum annealed, and then cold rolled in five passes using various lubricants. The thinnest strip, 0.66-0.69 mm thick, was obtained with the L2-203 lubricant, a synthetic compound of the type of complex esters containing amines. Castor oil and an LZ-171 lubricant were next in effectiveness. The rest of the



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SUB CODE: MH, IE NO REP BOY: 005 OTER: 000		ACCESSIO	n nr: A		ATD 1	RESS: 3108	encl: 00		
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PAVLOV, I.M.; DREGAN, I. [Dragan, I.]

Stu ies on the influence of reduction conditions in cold rolling on the magnetic and electric properties and the degree of perfection in the texture of transformer steel. Rev Roum metallurg 9 no. 1:75-85 '64.

32 EWP(k)/EWA(c)/EWT(m)/EWP(b)/T/EWA(d)/EWP(t) Pf-li L 34518-65 30 S/0000/64/000/000/0255/0262 MJW/JD/HW/GS ACCESSION NR: AT4048082 AUTHOR: Pavlov, I.M., Konstantinov, Ye. G., Taresevich, Yu. F., Shelest, TITLE: Investigation of the principal parameters of hot and warm rolling of several titanium alloys under peculiar conditions of stress SOURCE: Soveshchaniye po metallurgii, metallovedeniyu i primeneniyu titana i yego splavov. 5th. Moscow, 1963. Metallovedeniye titana (Metallography of titanium); trudy\* soveshchaniya. Moscow, Izd-vo Nauka, 1964, 255-262 TOPIC TAGS: titanium alloy, titanium alloy rolling, titanium alloy stress, titanium alloy plasticity/alloy OT4, alloy VT6, alloy VT14, alloy VT15, alloy VT1 ABSTRACT: The aim of this investigation was to study the plasticity, stress and deformation of titanium alloys on a "200" rolling mill (roll diameter 213 mm, rolling rate 0.5 m/sec, steel rolls) equipped with dynamometers for measuring the pressure on the rolls and torque meters for measuring the torque of the rolls. Type OT4, VT1, VT6, VT14 and VT15 alloys were selected; after being heated uniformly for 15-35 minutes, depending on the temperature of the rolls, the samples were rolled with an average compression of 20, 40 and 60% (with similar initial depth and variable final depth) at 500-1100C (every 100C). The tests showed that at rolling temperatures above 900C the specific Cord 1/3

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ACCESSION NR: AT4048082

pressure was relatively low. Only the VT15 alloy at a rolling temperature of 1100C and compression of 20% had a specific pressure of about 9 kg/mm<sup>2</sup>. The specific pressure increased more rapidly for the tested alloys than with technical titanium when the temperature dropped from 1100 to 900C. As the compression increased, the specific pressure increased due to friction. Lowering of specific pressure as the degree of deformation rises may be explained by crack formation in the metal line to unequal deformation because of the stressed condition in the narrow strips. This leads to higher lateral deformation in comparison with longitudinal deformation. The OT4, VT6, VT14 and VT15 alloys showed a lower plasticity than the VT1 alloy, the V#15 alloy having the lowest. The strips were widened by motion of the lateral surfaces into the contact surface, although widening was also caused by slipping along the contact surface, which was insignificant. Maximum widening at 20, 40 and 60% compression was obtained with Was insignificant. Maximum widening at 20, 40 and 00% compression was obtained with VT1 and VT15 alloys and at 900C with VT6 and VT14 alloys at 800C. As the degree of deformation increased, the widening rose for all alloys. Rolling of simples of various widths (8-60 mm) with 20% and 40% compression at 900C resulted in increased specific

ACCESSION NR: AT4048082  pressure together with the width, specific pressure increasing together with the midth increase. The curves in the paper show	
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pressure together with the width, specific pressure increasing by and in inverse proportion to width increase. The curves in the paper show and in inverse proportion to width increases absolute widening of the sample for all compression values first increases widths), reaches a maximum value, and then drops as the width increases	(for narrow
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AGGOGIATION. Laboratoriva plasticheskoy deformatsii Instituta metalluri	gii <u>im. A. A.</u>
Baykova (Laboratory of Plastic Deformation)	
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(N)

SOURCE CODE: UR/0000/66/000/000/0051/0055

AUTHOR: Pavlov, I. M.; Tarasevich, Yu. F.; Shelest, A. Ye.

ORG: none

TITLE: Deformations in the neck area of tensile-test specimens of certain titanium alloys

SOURCE: AN SSSR. Institut metallurgii. Napryazhennoye sostoyaniye i plastichnost' pri deformirovanii metallov (Stress condition and plasticity during metal deformation) Moscow, Izd-vo Nauka, 1966, 51-55

TOPIC TAGS: titanium alloy, tensile testing machine, tensile test, crystal orientation/ OT4 titanium alloy, VT6 titanium alloy, VT14 titanium alloy, IM-12A tensile testing machine

ABSTRACT: The deformations at the site of the greatest reduction in area of Ti (VT1) and Ti-alloy (OT4, VT6, VT14) test specimens in two mutually perpendicular directions were compared in order to indirectly obtain information on the anisotropy of mechanical properties. An IM-12A tensile testing machine was employed and the specimens were previously subjected to various types of thermomechanical treatment (rolling at 500 to 1100°C through every 100°C with reduction of area amounting to 20, 40 and 60% and with subsequent cooling in water, air and under asbestos). The criterion used to estimate deformation in the neck in two mutually perpendicular directions was the

Cord 1/2

ACC NR. AT7004415

difference between the maximum  $d_1$  and minimum  $d_2$  dimensions of the specimen's neck,  $\Delta d = d_1 - d_2$ . Findings: for technically pure titanium (VT1)  $\Delta d$  is virtually unaffected by the rate of cooling following rolling, and it increases with increase in reduction of area, particularly when the rolling temperatures are below 900°C. For the VT6 alloy  $\Delta d$  increases with decreasing temperature. For the VT14 alloy the maximum values of  $\Delta d$  are observed in most cases following treatment at 700-800°C. An analysis of the findings shows that the pattern of variation in  $\Delta d$  cannot be unambiguously related to the variation in mechanical properties of these alloys. On the other hand, it is interesting to note that, for all the alloys investigated, the position of the axes of  $\Delta d$  and  $\Delta d$  is uniquely determined by rolling temperatures: at 900-1100°C the maximum axis lies in the rolling plane, whereas at 500-800°C it extends in the perpendicular plane. This may be associated with the temperature dependence of crystallographic orientation: at 900-1100°C the alloys chiefly consisted of the  $\Delta d$ -phase with bcc lattice whereas the temperatures of 500-800°C pertained to the region of the existence of the  $\Delta d$ -phase with hexagonal lattice. Orig. art. has: 4 figures.

SUB CODE: 13, 20/ SUBM DATE: 27Sep66/ ORIG REF: 003

Cord 2/2

ACC NR: AT7004417

(N)

SOURCE CODE: UR/000/66/000/000/0086/0088

AUTHOR: Pavlov, I. M.; Mekhed, G. N.; Ch'ien Tseng-Shih

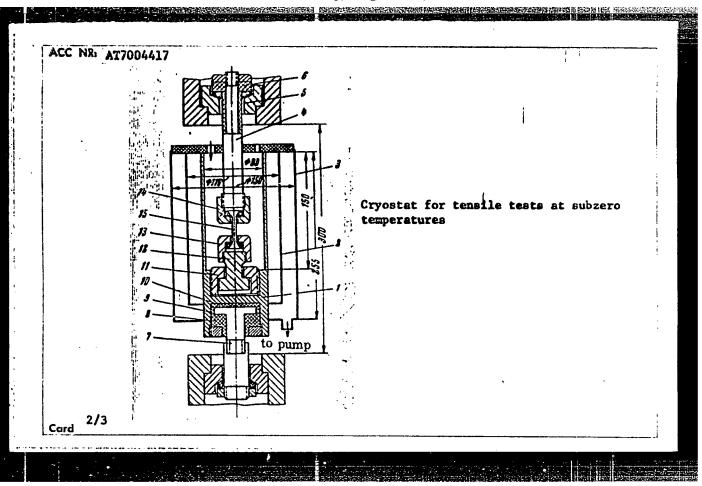
ORG: "Laboratory of Plastic Deformation of Metals, Institute of Metallurgy im. A. A. Baykov (Laboratoriya plasticheskoy deformatsii metallov Instituta metallurgii)

TITLE: Device for static tensile tests of metals and alloys at subzero temperatures SOURCE: AN SSSR. Institut metallurgii. Napryazhennoye sostoyaniye i plastichnost pri deformirovanii metallov (Stress condition and plasticity during metal deformation), Moscow, Izd-vo Nauka, 1966, 86-88

TOPIC TAGS: tensile test, static test, cryostat, metal test, low temperature research

ABSTRACT: Virtually every device for the tensile testing of specimens at low temperatures (reaching -196°C or even lower) is insufficiently airtight and involves leakage of coolant. This is because the specimen is linked to the lower clamp of the tensile testing machine by a long hose which passes through an opening in the bottom of the coolant container. In this connection, the authors developed in the Institute of Metallurgy im. A. A. Baykov a new improved device for tensile testing of specimens at temperatures as low as -268.8°C. The device (see figure) consists of a steel Dewar vessel containing the coolant mixture and hoses 4 and 7 attached to the clamps of the tensile testing machine. The Dewar vessel consists of three containers 1, 2, 3 of different diameters, inserted one in another. Impermost container 1 is filled with

Card 1/3



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with liquid helium, liquid nitrogen or a mixture of liquid nitrogen and gasoline, depending on the subzero temperature desired. During tests with liquid helium the space between the walls of containers 1 and 2 is filled with liquid nitrogen, while air is evacuated from the space between the walls of containers 2 and 3. With the nid of textolite attachments 6, 8, 9, 10 and wood tube 10 the coolant bath is specimen 15 is attached to hose 4 and work part 12 by means of nuts 13 and 14. Removal of the ruptured specimen and insertion of a new specimen are accomplished by turning work part 12 through 90° so as to release it from nut 11 which is constantly of coolant and assures an accurate and stable maintenance of the desired temperatures. Its design is simple and compact and it can be successfully operated as an attachment to an IM-12 type standard tensile testing machine. Orig. art.has: 1 figure.

SUB CODE: 13, 11/ SUBM DATE: 27Sep66/ ORIG REF: 016/ OTH REF: 009

**Cord 3/3** 

ACC NRIAT7004419

(A)

SOURCE CODE: UR/0000/66/000/000/0103/0106

AUTHOR: Pavlov, I. M.; Osipov, V. G.; Ushakov, Ye. V.

ORG: none

TITLE: Compressive tests at elevated temperatures

SOURCE: AN SSSR. Institut metallurgii. Napryazhennoye sostoyaniye i plastichnost' pri deformirovanii metallov (Stress condition and plasticity during metal deformation) Moscow, Izd-vo Nauka, 1966, 103-106

TOPIC TAGS: metal test, metallurgic research, compressive stress, temperature test

ABSTRACT: A new method of compressive tests of this kind is described. The tapered heads of specimen 1 (see figure) are inserted in the sockets of two dies having the same cone angle. To improve contact and eliminate the possibility of burnout, copperfoil linings 3 are inserted between the dies and platens 4. The current for heating the specimens is supplied to the platens via busbars 6. Coils 7 for the passage of water serve to prevent overheating of the dies. This device can be used to perform compressive tests of specimens at temperatures of up to 1000°C and it is superior to its previous counterparts in that it assures a greater uniformity of deformation of the specimen owing to a more uniform temperature field and stress-strain diagram in the middle cylindrical segment of the specimen. This is due to the presence of colder

Cord 1/2

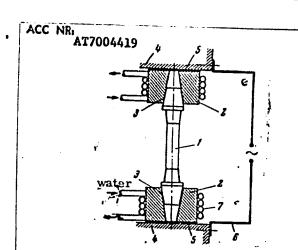


Fig. 1. Schematic of compressive test:

1 - specimen; 2 - die; 3 - lining;

4 - platen; 5 - lining; 6 - busbar;

7 - coolant coil

metal at both ends of the specimen and to the automatic decrease in current density in areas with higher temperature and increase in this density in areas with lower temperature; a rise in temperature in some cross sectional area of the specimen causes a decrease in deformation resistance in that area. (During compression the hotter sections of the specimen will undergo greater deformation, the cross sectional area of the specimen will increase and the current density will decrease.) A major advantage of this test method is the absence of any limitations on the heating temperature. Furthermore, it not only eliminates the adverse effect of friction forces on the uniformity of deformation but also preserves the strength of the press tools by preventing heat transfer from the test specimen to the tools. Orig. art. has: 6 figures.

SUB CODE: 13, 11/ SUBM DATE: 27Sep66/ ORIG REF: 003/

Card 2/2

ACC NR: AT7004426 (A) SOURCE CODE: UR/0000/66/000/000/0192/0195

AUTHOR: Pavlov, I. M. (Corresponding member AN SSSR); Mekhed, G. N.; Van Yu-Min

ORG: none

TITLE: Study of the effect of rolling temperature on the mechanical properties of high-strength steels following thermomechanical treatment

SOURCE: AN SSSR. Institut metallurgii. Napryazhennoye sostoyaniye i plastichnost pri deformirovanii metallov (Stress condition and plasticity during metal deformation). Moscow, Izd-vo Nauka, 1966, 192-195

TOPIC TAGS: steel, high strength steel, mechanical property, thermomechanical treatment/45KhNT steel, 60KhNYu steel

ABSTRACT: The mechanical properties of 45KhNT and 60KhNYu experimental high-strength steels subjected to a combination treatment of plastic deformation and quenching and tempering have been investigated. It was shown that these steels are characterized by a highly stable zone of supercooled austenite:

Card 1/2

UDC: 669.1

## ACC NR: AT7004426

500—600 C range for 45KhNT and above 400 C for 60KhNYu. Following thermomechanical treatment the mechanical properties of these steels are affected greatly by the rolling and tempering temperatures. An increase in rolling temperature decreases the hardness and strength of the steels and increases the plasticity. The optimum temperature for thermomechanical treatment is 500 C for 45KhNT and 500—600 C for 60KhNYu steel. Orig. art. has: 6 figures.

[AM] SUB CODE: 11,13/SUBM DATE: 27Sep66/ORIG REF: 005/OTH REF: 002/

Card 2/2

AUTHOR: P Van Y -Min	avlov, I.M. (Corresponding member AN SSSR); Mekhed, G.N.;
ORG: none	
low-temper	fect of the roller surface temperature and rolling speed in ature thermomechanical treatment on the mechanical properties and 60KhNYu steels
i plastich plasticity 199-202	N SSSR. Institut metallurgii. Napryazhennoye sostoyaniye nost' pri deformirovanii metallov (Stress condition and during metal deformation). Moscow, Izd-vo Nauka, 1966,
TOPIC TAGS	: high strength steel, and thermomechanical treatment, and
tarameter inter	: high strength steel, thermomechanical treatment, and the thermomechanical treatment; at the property, low alloy alloy at the steel, 60KhNYu steel
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hardness of 45 KhNT steel; however, the reduction of area increased from 11 to 22% and the elongation from 2.5 to 6%. Increasing the roller temperature from 20 to 250°C increased the tensile strength of 60KhNYu steel from 192-193 to 250 kg/mm<sup>2</sup>, the reduction of area from 3.4 to 9.5%, and the elongation from 0.6 to 4.7%; however, the changes in the yield strength and hardness were insignificant. The high strength and ductility of 60KhNYu steel can be explained by a more homogeneous martensitic structure resulting from rolling with hot rollers. The steels were also rolled with a 40% reduction at a constant roller surface temperature of 250-260°C at a rolling speed varying from 0.75 to 2 m/sec. Rolling in the 0.75-1.25 m/sec range of rolling speed was found to be the most effective. It increased the tensile strength of 45KhNT steel from 220 to 230 kg/mm<sup>2</sup>, the yield strength from 175 to 185 kg/mm<sup>2</sup>, and the reduction of area from 20 to 24%, but had practically no effect on the steel hardness and elongation. Similarly, the tensile strength of 60KhNYu steel increased from 237 to 243 kg/mm<sup>2</sup>, the yield strength from 163 to 171 kg/mm<sup>2</sup>, the reduction of area from 6.5 to 7%, the elongation from 2.3 to 3.5% and the RC hardness from 60 to 61.5 units. Further increases in the rolling speed had practically no effect on the mechanical properties of 45KhNT and 60KhNYu steels under the investigated conditions of thermomechanical treatment. Orig. art. has: 6 figures. [MS]

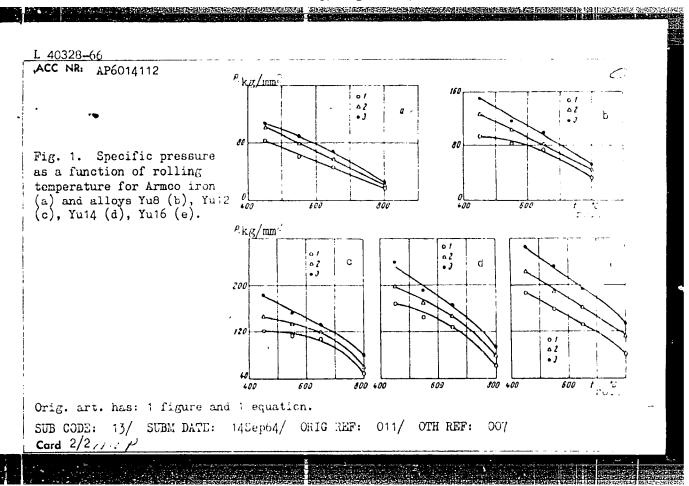
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300.32: Ref. zh. Mashinostr mat konstr i ran het detal minn. di rojr, eta bened.  MLF (CURCLE Tr. Monk. in-ta stall i relavov . Monk. energ. in-ta, vy). 40, 400 1, 1905, 199-179  10710 1AGS: From aluminum alloy, aluminum alloy projectly, audtlilly, sistemate diction.  ABSTRACT: Fe-Al alloys were studies with translating concentrations of occurrent 14.00 and 10.503 conditionally designated a 140, Volk. Yang and Yang respectively. Alloys with an aluminum concentration of 125 or more have low antillity of 15, 10% and and 2,41.3 ag/cm <sup>2</sup> ) and are brittle at rech temperature. The mechanical projection of
200. 32: Ref. zh. Mashinostr mat konstr i rad het detal mand. di rojr, 200. 32: Ref. zh. Mashinostr mat konstr i rad het detal mand di rojr, 200. 200. 200. 32: Ref. zh. Mashinostr mat konstr i rad het detal mand di rojr, 200. 200. 200. 200. 200. 200. 200. 200
ALT COURCE: Tr. Mosac.in-ta stellingplayov . Mosac. energ. in-ta, vyr. co., co. 1, 1965, 169-179  ABSTRACT: Fe-Al alloys were studies with the limiting concentrations of o.e., 1000 ind 10:000 conditionally designated a limit, Volume Yang unit Yang respectively. Alloys with an aluminum concentration of 12% or more have low dutility local, 1000 and alloys and are brittle at room temperature. The mechanical properties of
1965, 169-179  ICTIC TAGS: From aluminum alloy, aluminum alloy property, quetility, ultimate stronger  ABSTRACT: Fe-Al alloys were studied with the limiting concentrations of o.e., 1992  14.00 and 10.500 conditionally designated a 146, Yokay Yang unit The respectively.  Alloys with an aluminum concentration of 125 or more have low antillity forth, 1996  and apstraction. The mechanical properties of
ABSTRACT: Fe-Al alloys were studied with the inclinum concentrations of one of the land land of conditionally designated a land, Yok, Yok, and The respectively. Alloys with an aluminum concentration of 12% or more have low dustility longs, and and aluminum concentration of 12% or more have low dustility longs, and and applicable at reconstant transfer the mechanical properties of
14.00 and 10.500 conditionally designated a 140, Young Targuer
iron-aluminum alloys depend on temperature and aluminum constitution. There is sharp increase in strength characteristics at 100-200°C. The alloys may be divided into two groups on the basis of $\sigma_{\hat{b}}$ as a function of temperature. Alloys in the first
group (Yud and Yul2) show little change in o; (less than 4%). In the second prop
(Yul4 and Yul6) of increases (up to 40%) as the temperature is raised. Acres with
Cara 1/2 UDC: 5,405 UD

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ACC NR: AR0623314	
In aluminum concentration from 8 to 16.5% have two maxima on a curves.	
In the concentration of aluminum in the alloy is accompanied by a reduction in the first maximum (from 32 to 10 kg/cm $^2$ ) with a salit towers algaer temperature. This also to 450°C). At $600^{\circ}$ C, $\sigma_{\rm p}$ and $\delta$ are only slightly dependent on aluminum conventration	
and snow similar values for Yuō, Yul2 and Yul4 alloys. [Translation of abstract]	
SUB COLE: 11	
	-
Card 2/2 35	
CHU to / to V	

L 40328-66 EFT(m)/T/EFP(t)/ETT/EFP(k) LJP(c) ACC NR: AP6014112 (N) SOURCE	10/100 Table 10070 155 1000 1005 15075 10070
ACC NR. AP6014112 (N) SOURCE AUTHORS: Pavlov, J. M. (Moscow); Mekhed, G. N. (Moscow)	
ORG: none	
TITLE: Investigation of the hot-rolling process source: AN SSSR. Izvestiya. Metally, no. 6, 1965	of <u>iron-aluminum</u> alloys , 76-79
TOPIC TAGS: iron aluminum alloy, aluminum containmill, hot rolling / Yu8 iron aluminum alloy, Yu12 aluminum alloy, Yu16 iron aluminum alloy, duo 240 ABSTRACT: The specific rolling pressure of iron-Yu16 (containing 7.95, 11.55, 14.10 and 16.25% Al as a function of rolling temperature (300-8000) for Armco iron. Specimens (4 x 20 x 100 mm) were sheet and rolled on a duo 240 rolling mill at 0.6 tion during each pass). The results are shown in specific rolling pressure increases with aluminum temperature. During the rolling of aluminum allogicalificant difference in rolling pressure was fo the order-disorder transition temperature.	ron aluminum alloy, Yu14 fron rolling mill  27 27 27 aluminum alloys Yu8, Yu12, Yu14, and by weight respectively) was measured and compared with the rolling pressure cut from hot-rolled (100010500) 3 m/sec in three passes (10% deforma- Fig. 1. It was found that the content and decreases with rolling ys having long-range order (no
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### "APPROVED FOR RELEASE: Tuesday, August 01, 2000

CIA-RDP86-00513R001239

 $\operatorname{ExT}(d)/\operatorname{ExT}(m)/\operatorname{ExP}(w)/\operatorname{ExP}(v)/\operatorname{T/ExP}(t), \operatorname{cli/ExP}(k)/\operatorname{Exi}(h)/\operatorname{ExP}(1)$ ACC NR. AT6012409 SOURCE CODE: UR/0000/65/000/000/0312/0316 AUTHORS: Pavlov, I. M.; Konstantinov, Ye. G.; Shelest, A. Ye.; Tarasevich, Yu. F. ORG: none TITLE: Several rolling conditions for titanium alloys SOURCE: Soveshchaniye po metallokhimii, metallovedeniyu i primeneniyu titana i yego splavov, 6th. Novyye issledovaniya titanovykh splavov (New research on titanium alloys); trudy soveshchaniya. Moscow, Izd-vo Nauka, 1965, 312-316 FRICTION QUEFFICIENT, TOPIC TAGS: A metal rolling, titanium alloy, rolling mill, metal friction / VT1 titanium alloy, OT4 titanium alloy, VT6 titanium alloy, VT14 titanium alloy, VT15 titanium alloy, duo 200 rolling mill ABSTRACT: The coefficient of external friction during rolling of rectangular titanium alloy slabs under a wide range of temperature and deformation conditions was investigated. Specimens (12 x 10 x 150 mm) of titanium alloys VT1, 074, VT6, VT14, and VT15 were preheated to 500--1100C (at 100C intervals), rolled on a duo 200 rolling mill with relative reductions of 20, 40, and 60%. The forward flow and coefficient of friction were measured and tabulated for these rolling conditions. The coefficient of friction over the temperature interval 500--11000 was found to be ≈ 0.15, while the forward flow was found to vary considerably. Curves of the forward flow and friction coefficient as a function of strip width are presented for alloy VT6 (20 and 40% **Cord** 1/2

CC NR. AT601240	9				0	
21 - 45 224	ng torque on a	single roll as vestigation can	a function of be used to d	width. An equat of rolling paramet etermine rational and 1 table.	ALR TR	
7B CODE: 11, 13	/ SUBM DATE:	O2Dec65/ ORIG	REF: 003			
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CIA-RDP86-00513R001239

ACC NR. AT6012386 AUTHORS: Pavlov, I. M.; Shelest, A. Ye.	SOURCE CODE: UR/OOOO,	, ->, -00, 000, 01	
RG: none		OF SERVICE	58 54 B+1
		•	011
ITLE: Peculiarities of gas saturation of	Some titanium alloys	_19	
OURCE: Soveshchaniye po metallokhimii, m			
splavov, 6th. Novyye issledovaniya titanov alloys); trudy soveshchaniya. Moscow, Izd-	rykh splavov (New reservo Nauka, 1965, 163-16	arch on titanio	um -
HARDNE 539			
OPIC TAGS: stitanium, titanium alloy, gas as diffusion, temperature/ VTl titanium,	s absorption, plasticit OThel titanium alloy.	ty, phase compo OTA titanium a	osition,
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To titanium alloy, VT14 titanium alloy, V	T15 titanium alloy	<i>'</i>	
T6 titanium alloy, VT14 titanium alloy, V	TIS titanium alloy	** * **	ed.
BSTRACT: The characteristics of gas satu	T15 titanium alloy $\gamma$ ration of titanium all	loys are studie	ed. . G.
BSTRACT: The characteristics of gas satured by The work is based on an earlier study by The constanting (Osobennosti okisleniya nekot	TT15 titanium alloy of the second of titanium alloy of the second of titanium alloy	loys are studio nelest, and Ye, yov ppi nagreye	. G. e pered
BSTRACT: The characteristics of gas satured by The work is based on an earlier study by The constanting (Osobennosti okisleniya nekot	TT15 titanium alloy of the second of titanium alloy of the second of titanium alloy	loys are studio nelest, and Ye, yov ppi nagreye	. G. e pered
BSTRACT: The characteristics of gas satu The work is based on an earlier study by I	ration of titanium alloy ration of titanium allow. A. Ye. Shorykh titanovykh splayego polavyk Metallovec	loys are studio nelest, and <u>Ye</u> yov ppi nagreve denise titana, <u>7115</u> were studi	. G. e pered Izd-vo ied.
BSTRACT: The characteristics of gas satured work is based on an earlier study by I constantinov (Osobennosti okisleniya nekot lasticheskoy deformatsiyey. So. Titan i yaka, 1964). Titanium alloys VTI, OTL-1	ration of titanium alloy ration of titanium allow. A. Ye. Shorykh titanovykh splayego polavyk Metallovec	loys are studio nelest, and <u>Ye</u> yov ppi nagreve denise titana, <u>7115</u> were studi	G. pered Izd-vo ied.

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CIA-RDP86-00513R0012396

29920-66 EWP(k)/ENT(m)/T/EWP(w)/EWP(t)/ETI IJP(c) DJ/JD/HN/JG AP6017300 (A, N) ACC NRI SOURCE CODE: UR/0136/66/000/005/0093/0094 AUTHOR: Krupin, A. V.; Pavlov, I. M.; Linetskiy, B. L.; Chernyshev, V. N.; Zarapin, Yu. L.; Starkov, V. N.; Korchagin, P. A.; Vinogradov, V. V.; Tyukalov, T. V. E ORG: none TITLE: Rolling of tungsten and molybdenum under conditions of low partial pressures of oxygen SOURCE: Tsvetnyye metally, no. 5, 1966, 93-94 TOPIC TAGS: tungsten, molybdenum, hot rolling, tungsten rolling, molybdenum rolling, vacuum rolling ABSTRACT: Tungsten and molybdenum practices (8 x 40 x 150 mm) preforged or prerolled from sintered ingots were hot rolled in air, argon containing 0.03%  $0_2$  and 0.01%  $N_2$ . or in a vacuum of 0.1-0.005 mm Hg. Tungsten was rolled at 1200,  $1300^2$ , and 1450C with reductions of 10, 20, and 30% per pass; molybdenum was rolled at 950, 1050, and 1150C with reductions of 10, 20, 30, 50, and 55% per pass. A sharp increase in the roll pressure, torque, forward slip, and friction coefficient as observed with change from air atmosphere to a pressure of 0.1 mm Hg. This was caused by creased friction. Lowering the pressure from 0.1 to 0.005 mm Hg had little or no additional effect. Increasing the rolling temperature in vacuum of 0.01 mm Hg had an insignificant effect on the specific pressure in rolling molybdenum, but appreciably Cord 1/2 UDC: 669.27/.28:621.771

# **的专利基础的原理的现在分词是** L 29920-66 ACC NR: AP6017300 decreased the specific pressure in rolling tungsten, e.g., from 74 At 1200C to 64 and 60 kg/mm<sup>2</sup> at 1300 and 1450C, respectively. The specific pressure increased with increasing reduction. In rolling tungsten in a vacuum of 0.1 mm Hg, increasing the reduction from 20 to 30% led to a specific pressure increase from 74 to 91 kg/mm<sup>2</sup> at 1200C and from 60 to 69 kg/mm<sup>2</sup> at 1450C. In rolling molybdenum the specific pressure increased from 44 to 96.5 kg/mm<sup>2</sup> with increasing reduction from 10 to 45% at 1050C. In vacuum rolling at high temperatures and reductions a sticking of metal to the rolls was observed. In rolling of tungsten at 1450C with a reduction of 35%, an intensive sticking resulted in splitting of metal. Little or no sticking was observed at 1200C. Noticeable sticking was observed in rolling molybdenum at 1150C. [MS] SUB CODE: 11,13/SUBM DATE: none/ ORIG REF: 001/ ATD PRESS: 501/ Card 2/2

PAYLOW, I.M. (Moskva); MEKHED, G.N. (Moskva); NEWOROV, V.A. (Moskva);

TARASEVICH, Yu.F. (Moskva)

Investigating the warm rolling of iron-aluminum a loys. low
AN SSSR. Met. no.6:76-79 N-D 'rol.

1. Submitted September 14, 1964.

	24864	UR/0136/65/000/010/0083/00 669.2/.8:621.771.2
AUTHOR: Pavlov, I.I	M.; Koryagin, N.I.	-31
TITLE: Natural con	ditions of roll bite during	the rolling of multilayer metals
BOURCE: Tavetnyye	metally, no. 10, 1965, 83-86	<b>4</b> ,55, 1.5
TOPIC TAGS: metal:	rolling, metal friction, fri	ction coefficient
ABSTRACT: Roll bite	e requires that the horizont of metal in between the rol	al friction force exceed the force ls. For metals whose surface in coefficients this can be described
contact with the roll by a relatively sim	ple formula, but for multi-lemula is derived by the authorized	aver metals a special formula is

L 3496-66

ACCESSION NR: AP5024864

where f<sub>1</sub> is the friction coefficient of one metal surface, f<sub>2</sub> is the friction coefficient of the other metal surface, and a is the angle of bite. On this basis, it is shown that in the rolling of multilayer packets with contact surfaces having different friction coefficients, the maximum bite angle of the packet is roughly determined by the expression

$$tan \frac{\beta_1 + \beta_2}{2} \approx tan. \sigma$$
 (2)

where  $\beta$ ,  $B_2$ , are the friction angles. Or, on replacing the friction angles with the maximum bite angles, we have

$$\frac{a_1+a_1}{2}\approx \alpha.$$
 (3)

It is further shown that in the case of a multilayer-metal billet, roll bite does not necessarily require the application of an external push. This is documented by

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L 3196-66 ACCESSION NR: AP5024864

experiments with the cold rolling of two-layer (layers of 3 mm each) billets measuring 3x375x375, with reduction of area from 6 to 2.5 mm, 1.e., with a bite angle of 6°10', by the following procedure: with the rolls halted, the billets were placed in a position ready for bite (a), whereupon the rolls were put in motion and roll bite took place (b) (see Fig. 1 of the Enclosure). This experiment shows that it is sufficient for the layers of the metal to come into contact with the rolls in order to immediately generate the force R sufficient to form a friction force capable of entraining the billet into the zone of deformation without the application of an external push. The second part of the experiments pertained to the determination of bite angles during the hot, cold, and combined hot-cold rolling of two- and multi-layer metals with the rolls treated with different solutions or lubricants The findings confirmed the validity of formula (3), i.e., the maximum bite angle of a multilayer packet with different friction coefficients of the packet's components is determined with sufficient accuracy according to their respective bite angles. Orig. art. has: 1 figure, and 5 formulas.

ASSOCIATION: none

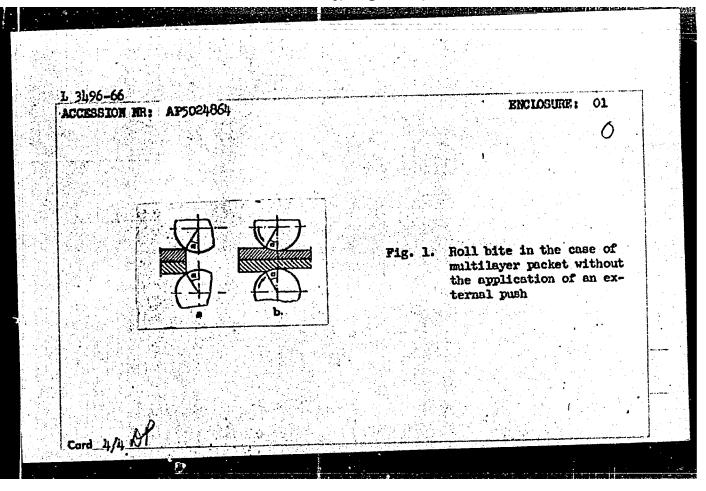
SUBMITTED: 00 NO REF SOV: 007

ENCL: O1 OTHER: 000 SUB CODE: MM, IE

Cord 3/4

APPROVED FOR RELEASE: Tuesday, August 01, 2000

CIA-RDP86-00513R0012396



PAVIOU, T.M.; AVRUNIN, P.M.

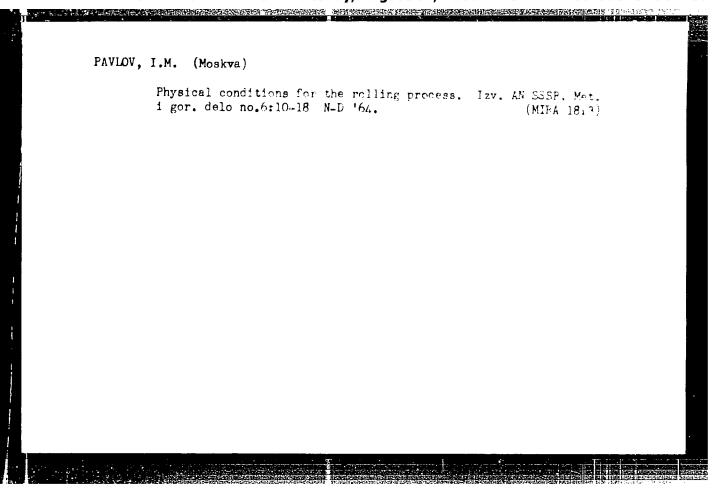
Investigating the longitudinal and transverse effectiveness of deformation during rolling. Izv. vys. ncheb. zav.; chern. met. 8 no.9192-97 165. (MIRA 18:9)

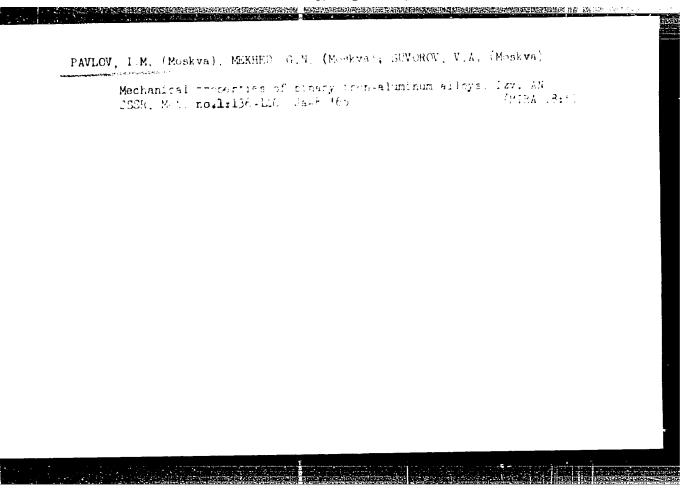
1. Moskovskiy institut stalt i splavov.

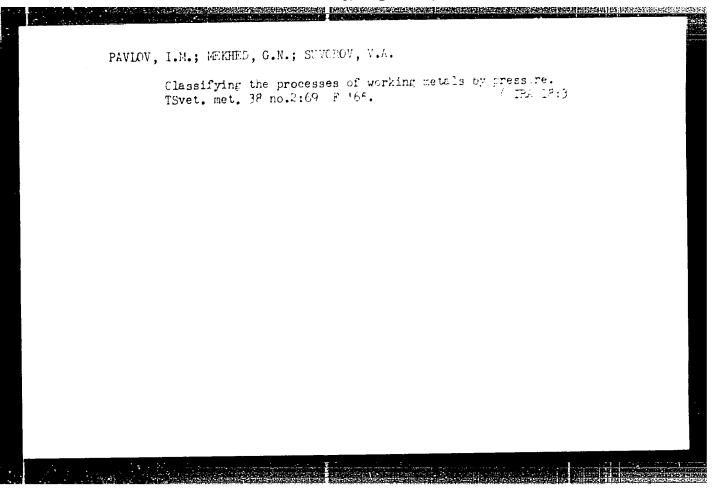
PAVLOV, I.H. (Moskva)

Conditions for plastic deformation in connection with certain vector relations. Izv. AN SSSR. Met. no.3:89-100 My-Je '65.

Physical conditions for plastic deformation in the aspect of certain general correlations between motion and friction. Ibid.:73-85
65. (MIRA 18:7)







BENEVICE STREET, STREE

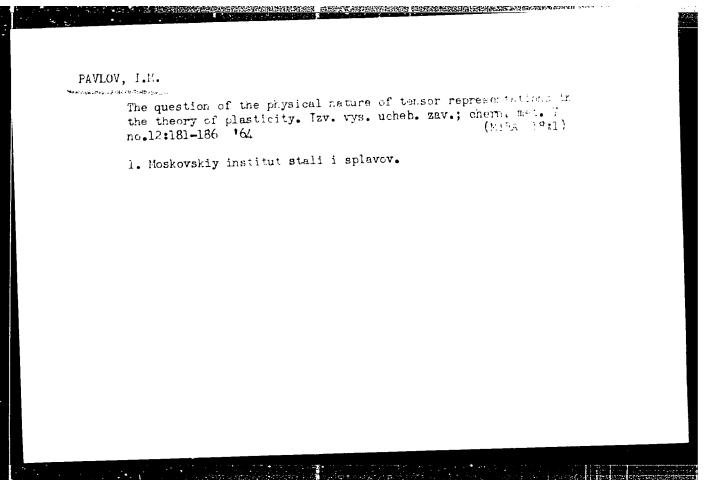
PAVLOV, I.M.; KOROLEV, A.A.; ILKA IOAN; CHERNYSHEV, V.N.

Device for the investigating of the asymmetrical process of longitudinal rolling. Izv. vys. ucheb. zav.; chern. met. 7 no.11:105-111 '64. (MIRA 17:12)

l. Moskovskiy institut stali i splavov.

L 12961-65 ENT (d)/ENT (m)/EPF (n)-2/ENG (m)/ENA (d)/EMP (v)/EPR/ENP(t)/EMP (k)/EMP (h)/ EWP(z)/EMP(b)/EWP(l)/EWA(c) Pf-L/Ps-L/Pu-L LJP(c) JD/HM/JG \$/0148/65/000/003/0089/0093 ACCESSION NR: AP5008388 AUTHOR: Krupin, A. V.; Pavlov, I. H.; Chernyshev, V. N.; Bogolyubov, V. S.; Linetskiv, B. L. TITLE: The vacuum rolling mill 210 SOURCE: IVUZ. Chernaya metallurgiya, no. 3, 1965, 89-93 TOPIC TAGS: vecuum rolling mill, rolling mill equipment, rolling mill 210 ABSTRACT: The vacuum rolling plant 210 has been designed and built at the Moscow Institute for Steel and Alloys. The plant consists of a rolling mill and heat-treating furnaces enclosed in a common vacuum chamber, which makes it possible to heat, roll, and heat-treat metals and alloys either in a vacuum or in a protective atmosphere in one continuous operation. The one-stand, two-high reversible mill has rolls 210 mm in diameter and 340 mm long. The maximum permissible roll pressure is 100 tons, and the maximum roll opening is 50 mm.
The mill is driven by a 22-kw, d-c motor at speeds of 400 to 1000 rpm. The rolls can be preheated if necessary. The maximum temperature in Card 1/2

42964-65 CCESSION NR: AP5008388	
020 mm in diameter and i acuum system can evacuat ill has been used to rol	in another, 1300C. The vacuum chamber is smade of a steel plate 10 mm thick. The e the chamber to $1 \cdot 10^{-2} - 1 \cdot 10^{-5}$ mm Hg. The l refractory metals ( $(\sqrt{27} \text{Nb})^2 \text{Ta}, \sqrt{27} \text{Mo}$ ) and inates (e.g., titanium alloy-bronze, titanium tanium alloy-niobium-stainless steel, titanium
lloy-stainless steel, tl lloy-tantalum-stainless	institut stali i splavov (Moscow Institute
lloy-stainless steel, ti lloy-tantalum-stainless SSOCIATION: Moskovskiy or Steel and Alloys)	steel). Orig. art. nas: 1 ligo.c.
lloy-stainless steel, ti lloy-tantalum-stainless SSOCIATION: Moskovskiy	institut stali i splavov (Moscow Institute



L 45062-65 ENT(m)/EPF(n)-2/EMA(d)/T/EMP(t)/EMP(k)/EMP(z)/EMP(b)/EMA(c) Pf-4/
Pu-4 LJP(a) MJW/JD/EM/JG
ACCESSION NR: AR5008958 S/0277/65/000/001/0025/0025

SOURCE: Ref. zh. Mashinostroitel'nyye materialy, konstruktsii i raschet detaley mashin. Otd. vyp., Abs. 1.48.125

AUTHOR: Paylov, I. M.; Danil'chenko, A. N.; Rastegayev, M. V.; Mezis, V. Ya.; Napalkov, L. A.; Kulechov, M. Ya.

TITLE: A study of plasticity and microstructure of VM-2 alloy when deformed by upsetting

CITED SOURCE: Tr. Mosk, in-ta metallurgii, Mosk, energ, in-ta i Mosk, in-ta stali i splavov vyp. 44, 1963, 256-263

TOPIC TAGS: molybdenum alloy, alloy plasticity, alloy microstructure, hot upsetting, bulge test, optimum deformation temperature, VM-2 alloy

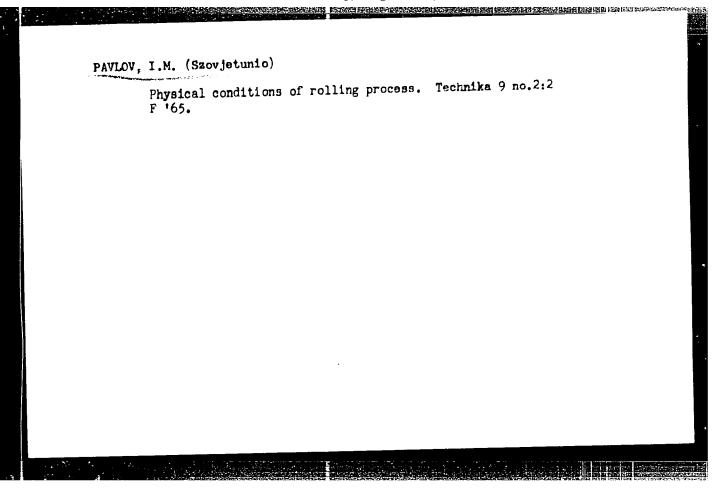
TRANSLATION: The report gives the results of a study of the plasticity and microstructure of VM-2 molybdenum alloy after upsetting! The alloy's mechanical properties at room temperature were: 0.2 = 27.2 - 28.0 kg/mm², Sc = 37.0 - 41.0 kg/mm², S = 6-107, T = 5-8.5%. Samples with diameter = 20 mm were bulge-tested on a 450 kg-m vertical impact tester with a max, ram drop rate of 10 to Cord. 1/2

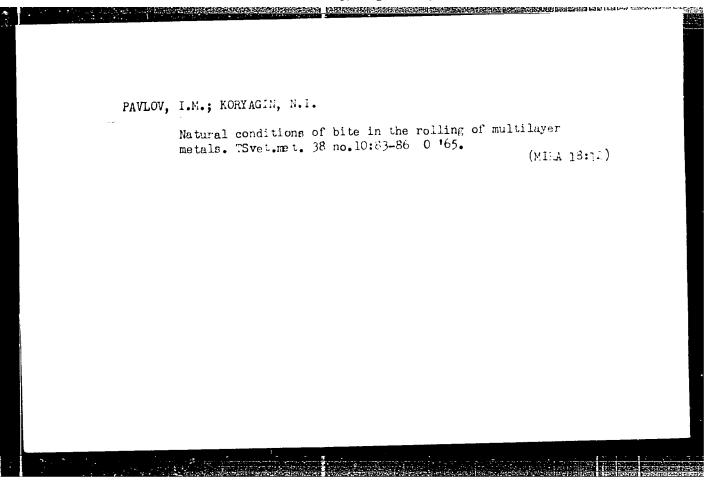
pressed and annealed statemetry to levels of 70% with vere also absen+in diamete	al grades of VM-2 alloy exhibit adequate plasticity in te. The samples were upset along the axis of symhout the development of cracks at 800-1400C. Cracks er reduction (spread) to max, deformation of 55-58% arred only when upsetting at 500-700C. A comparison of for every and upsetting at 900-1200C has shown that	
ffective pressure values of this characteristic teaches this characteristic teaches this characteristic teaches this characteristic teaches the commendation of the characteristic teaches the characteristic teac	es levels higher by 10-40% for VM-2 alloy than for stee conditions being equal. Deformation temperatures of led in relation to alloy VM-2. Bibl. with 3	ls
SUB CODE: MM		7
UB CODE: MM		

L 45459-65 ENT(m)/ENA(d)/EPR/ENP(t)/ENP(k)/ENP(z)/ENP(b)/ENA(c) Pf-4/Ps-4 IJP(c) MJW/JD/HW -UR/0370/65/000/001/0136/0140 ACCESSION NR: AP5009269 AUTHOR: Pavlov, f. M. (Moscow); Makhad, G.N. (Moscow); Suvorov, V.A. (Moscow) TITLE: Mechanical properties of binary iron-aluminum alloys SOURCE: AN SSSR. TOPIC TAGS: alloy mechanical property, binary alloy, iron alloy, aluminum alloy, alloy plasticity 4 ABSTRACT: This paper/is devoted to a/study of the temperature dependence of the mechanical properties of Fg-Al alloys containing 8, 11.5, 14, and 16.5% Al and designated Yu8) Yu12, Yu14, and Yu16, respectively. The alloys were prepared in a magnesite crucible by fusion in a vacuum finduction furnace of the TSNIIChM experimental plant, using armoo iron and AVOOO aluminum. All the alloys except Yu8 had a low technological plasticity  $() \angle 5\%)$  at room temperature. The strength of all the alloys was between 48 and 68 kg/rm<sup>2</sup>. It was found that as the temperature rose from 25 to 300-400 C, after a certain dip, a sharp rise in the ultimate strength was observed, particularly in alloys Yul4 and Yul6. The maximum strength in Yus and Yul2 was observed at 3000, and in Yul4 add Yul6, at 4000; the greatest

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trength was displayed by a		11		1.0		A 4	.	• , • -
	lloy Yui4, W	hich had ar	riging	tempo	structure. rature DT(	omotes (	an.	
strength was displayed by a crease in the plasticity of Increase in strength. The	4 A R P C A A A A A A A A A A A A A A A A A A	'no grrenga.		T	7777 V V V V V V V V V V V V V V V V V	,		
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EMT(m)/EMP(w)/EMA(d)/T/EMP(t)/EMP(k)IJP(c) SOURCE CODE: UR/0136/66/000/004/0072/0073 22347-66 ACC NR: AP6012728 AUTHOR: Pavlov, I. M.; Burkhanov, S. F.; Shor, E. R.; Osipov, E. Ye.; Chimenov, A. ORG: none TITLE: Study of resistance to deformation during cold rolling of VT14, VT15, and VT16 alloy strips SOURCE: Tsvetnyye metally, no. 4, 1966, 72-73 TOPIC TAGS: titanium, titanium alloy, titanium alloy strip, strip rolling, cold rolling, titanium clad alloy/VT14 alloy, VT15 alloy, VT16 alloy ABSTRACT: The roll pressure and resistance to deformation during cold rolling of clad and unclad VT14, VT15, and VT16 titanium alloy strips has been investigated. Unclad 1.8 x 250 x 500 mm strips were rolled into strip 1 mm thick at a rate of 30-90 m/min with a reduction of 3-6% in the first and 1-2% in the final passes. All the alloys were relatively easily reduced in the first passes, but in the last passes the edges of VT14 alloy strip began to tear at 40% total reduction. Rolling of this alloy was accompanied by intensive strain hardening. VT15 alloy had less resistance to deformation than VT14 alloy. The lowest pressures were required for VT16 alloy. The average pressure at 30% reduction was 230 kg/mm<sup>2</sup> for VT14 alloy, 220 kg/mm<sup>2</sup> for VT15 alloy, and 180 kg/mm<sup>2</sup> for VT16 alloy. Alloy strips clad on each side with VTl commercial-grade titanium were easily reduced to 30-40% of the UDC: 669.295-124.2:620.1

1 22347-66 ACC NR: AP6012728				
tion of clad and v	with the average practice action action with the action action action with the action action action with the action actio	erties. Clad	decreased by 30 ding significant	
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L 45294-66 EWP(e)/EWP(v)/EWT(d)/EWT(m)/T/EWP(t)/ETI/EWP(k)/EWP(h)/EWP(1) IJP(c) ACC NR. AR6017489 JD/HW/JG/AT/WH SOURCE CODE: UR/O137/66/000/001/D024/D024	
AUTHORS: Pavlov, I. M.; Krupin, A. V.; Chernyshev, V. N.; Bogolyubov, V. S.;  Linetskiy, E. L.  TITLE: Devices for working refractory metals in vacuum and in inert media	
SOURCE: Ref. zh. Metallurgiya, Abs. 10170  REF SOURCE: Tr. Mosk. in-ta stali i splavov i Mosk. energ. in-ta, vyp. 61, ch. 2,	
TOPIC TAGS: physical metallurgy, metal rolling, rolling mill, refractory metal	
ABSTRACT: Problems associated with rolling some metals in a vacuum are discussed.  Special types of mills used in vacuum rollinguand the technique of rolling some refractory metals are described. A. Leont'ev Translation of abstract  SUB CODE: 11	
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Card 1/1 /// UDC: 669.621.771.27	

ACC NR: AP6019767 (	/T/EMP(t)/ETI/EMP(k) IJP(c) JD/HW/JH A) SOURCE CODE: UR/0370/66/000/003/0090/0093
(المنصر) AUTHOR: Pavlov, I. M.; Mekh	(Moscow)  18d, G. N.; Suvorov, V. A. (Moscow)  48
ORG: none	
TITLE: Effect of roll tempe inum alloys	rature on specific pressure in the rolling of iron-alum-
SOURCE: AN SSSR. Izvestiya	. Metally, no. 3, 1966, 90-93
TOPIC TAGS: rolling mill, h	not rolling, cold rolling, chemical composition wok
aluminum alloy, temperature	
ABSTRACT: The problem of re	ducing the cooling effect of rolls on metal being rolled
	given temperature is discussed. A gas-fired Duo 240
	es of ordered, magnetic Fe-A/ alloys (Yu8 7.95% A/, Yu12 D
	ul6 16.25% A/), all of which, with the exception of Yu8,
	e alloys are body-centered cubic in structure and those
	are brittle at room temperature and cannot be cold rolled.
	also rolled for purposes of comparison. Two series of ven temperature in two stages; one series on cold rolls,
-	ed to 250°C. From plotted data it was noted that specific
	old rolls. The magnitude of specific pressure lowering for
<u>.</u>	ed rolls, as compared with cold rolls, depended on aluminum
	the different values for the friction, coefficients for
,	
Card 1/2	UDC: 621.771.001

L h5h36-66

### ACC NR. AP6019767

differing aluminum content and by the abrupt cooling of the rolled metal on cold rolls. Physical properties of the surface layers, and differences in chemical composition of scale, lead to change in friction coefficients. The data cited make it quite evident that warm rolling of Fe-A/ alloys on hot rolls significantly reduces the degree to which they are strengthened. Magnitudes of specific pressures obtained in the rolling of Yu12, Yu14, and Yu16 alloys on rolls heated to 250°C after the third pass were almost the same as those for the alloys after the second pass when processed on cold rolls. The rolling of metal on hot rolls makes it possible to reduce the number of passes required in rolling Fe-A/ alloys. Roll wear is decreased, an important factor in the rolling of these alloys. Org. art. has: 5 sets of curves.

SUB CODE: 11, 13/ SUBM DATE: 31 May 65 / ORIG REF: 010

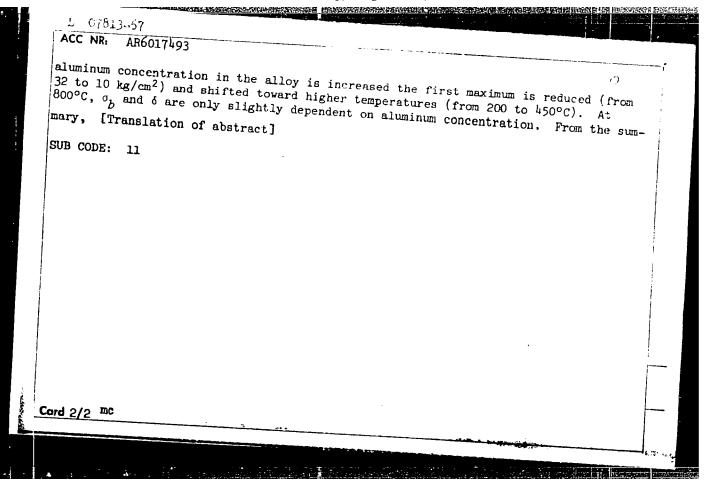
Card 2/2

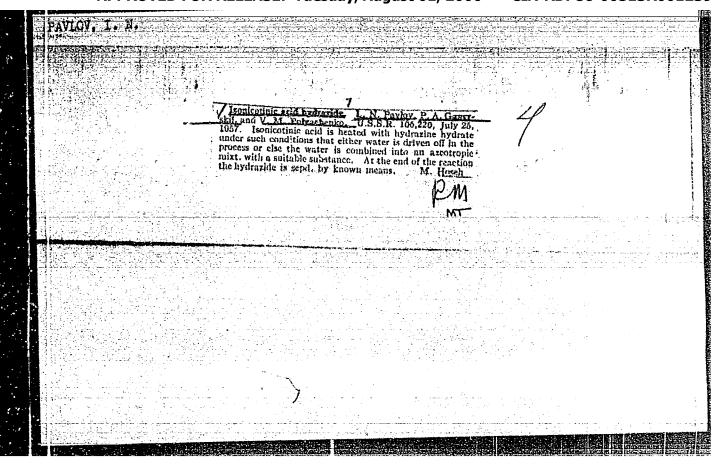
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L 07815-67 EWT(m)/EWP(t)/ETI/EWP(k) IJP(c) FDN/JD/HW  ACC NR: AR6017480 SOURCE CODE: UR/0137/66/000/	OO1/DOO7/DOO8
AUTHOR: Pavlov, 1. M.; Konstantinov, Ye. G.; Shelest, A. Ye.;	Tarasevich, Yu. F.
TITLE: Conditions for hot and warm rolling of some titanium al	Lloys 28
SOURCE: Ref. zh. Metallurgiya, Abs. 1D42	3
REF SOURCE: Tr. 40sk. in-ta stali i splavov i Mosk energ. in-t	a, vyp. 61, ch. 1,
TOPIC TAGS: hot rolling, warm rolling, titanium alloy	
ABSTRACT: It was found during this investigation that an incre $H=$ const) increases the widening index for all alloys studied, we ally due to barrel distortion. Due to the narrow width of the conditions of this investigation, transverse deformation $\Psi=B_2/B$ gitudinal deformation $\mu=L_2/L_1$ in nearly all cases, which correstar conditions for the stressed state of the metal at the source increase in reduction resulted chiefly in development of transverse to drawing deformation. A. Leont'yev. [Translation of all	specimens under the laws greater than lon- ponded to the particu- e of deformation. An erse deformation rela-
SUB CODE: 13, 1/	
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Card 1/1 mc	DC: 621,771,001

L 07813-67 EWT(m)/EWP(w)/EMP(t)/ETI IJP(c) JD/JH
ACC NR: AR6017493 SOURCE CODE: UR/0137/66/000/001/1071/1072
AUTHOR: Pavlov, I. M.; Mekhed, G. N.; Suvorov, V. A.  TITLE: Effect of temperature on the mechanical properties of iron-aluminum alloys
SOURCE: Ref. zh. Metallurgiya, Abs. 11479
REF SOURCE: Tr. Mosk. in-ta stali i splavov i Mosk. energ. in-ta, vyp. 61, ch. 1, 1965, 169-179
TOPIC TAGS: iron aluminum alloy, metal stress, solid mechanical property  ABSTRACT: Yu8, Yu12, Yu14 and Yu16 Fe-Al alloys were studied with aluminum concentrations of 8.0, 11.5, 14.0 and 16.5% respectively. The alloys have low ductility ( $\delta < 5\%$ , $\psi < 5\%$ , $a_k < 1.3 \text{ kg/cm}^2$ ) at room temperature. The mechanical properties depend on temperature.
ature and aluminum concentration. Strength increases sharply at 100-200°C. The alloys studied were divided into two groups according to the nature of variation in the with respect to temperature. In the first group are Yu8 and Yu12 which show little
change in $\sigma_b(<4\%)$ . In the second group are Yull and Yul6 which show a considerable
increase in $\sigma_b$ (up to 40%) as temperature is raised. Alloys with 8-16.5% aluminum con-
centration have two maxima on curves for $a_k$ as a function of temperature. As the
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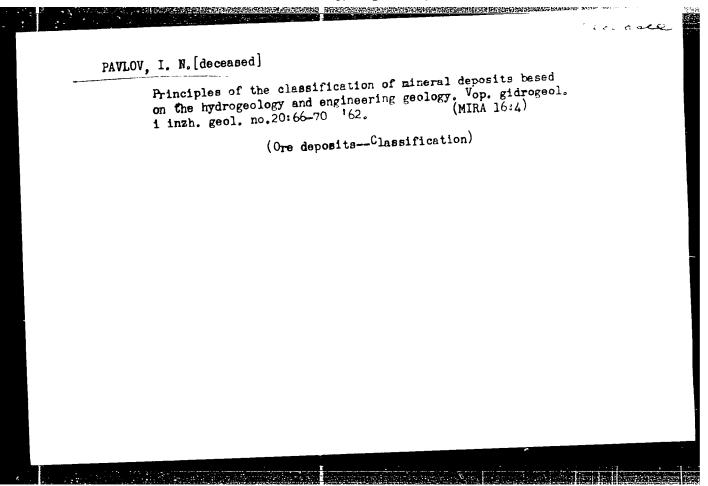


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PAVLOV, I.B. [deceased]; PROKHOROV, S.P.; SKVORTSOV, G.G.; LOSEV, F.I.,
Prinimali uchastiye: ROMANOVSKAYA, L.I.; KISSIN, I.G.; KULIBABA,
F.V., FILIPPOVA, B.S., red.; IVANOVA, A.G., tekhn.red.

[Iron ore deposits in the Kursk Magnetic Anomaly from the point of view of hydrogeology and engineering geology] Oidrogeologi-cheskie i inzhenerno-geologicheskie usloviis zhelezorudnykh mestorozhdenii Kurskoi magnitnoi anomalii. Moskva, Gos.nauchnotekhn.izd-vo lit-ry po geol. i okhrane nedr. 1959. 271 p. (MIRA 13:3)

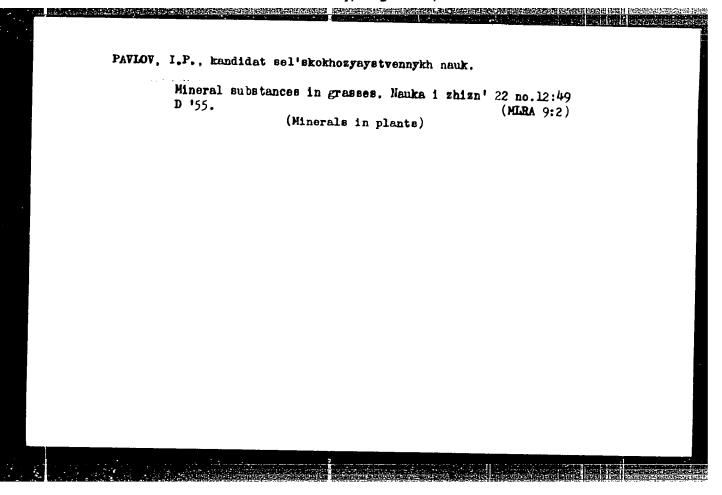
(Kursk Magnetic Anomaly--Iron ores)



- PAVLOV, I. P.
- USSR (600)
- Feeding and Feeding Stuffs Analysis
- Yield and nutritive value of green fodder from a mixture of vetch and oats at different stages of development. Sov. zootekh. 7/No.3,1952. Kandidat Sel'skodhozyatst-vennykh Nauk Vsesoyuznyy Nauchno-Issledovatel'skiy Institut Kormleniya
- 9. Monthly List of Russian Accessions, Library of Congress, June 1952. Unclassified Sel'skokhozyaystvennykh Zhivotnykh

PAVLOV, I. P.	
Voeds	
Wild oats and ways of fighting them; Sov.	agron. 10 No. 3, 1952.
9. Monthly List of Russian Accessions	, Library of Congress, May 1952. 1998, Uncl.

	PAVLOV , Im. R
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	13559 (Increasing Nutrition Value of Grasses.) Povyalvente
	13559* (Increasing Nutrition Value of Grasses.) Povyal ente pitatel'nosti kormovykh trav. I. P. Pavlov. Dastizhenia Nauki i Poredovogo Opyta v Selskom Kravanstie, 1054, no. 6, June,
	p. 14-15. Effect of fertilizers on protein content of vetch-oat hay. Tables.
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Country : USSR

Category: Cultivated Plants Grains.

Abs Jeur: RZhBiol., Mc 11, 1958, No 48871

..uchor : Pavlov, I.P.

: Sci. Res. Inst of Foodstuffs for Agricultural Last

Animals.

: Corn in the " n-Chernozem Belt. Title

Orio Pub: Vestn. s.-1' naulhi, 1956, No 3, 75-64

Abstract: This article describes the results of experients

on growing the following corn varieties: Sterling Krasnodarskiy, Krasnodarskaya 1/49. Li. 10 Kubaskiy and Moskovskinga Populyatsiya. The experiments were conducted during 1954-1955 at the All-Union Scientific Research Institute of Foodstuffs for Gricultural Animals (near Mescow). The early sowings of corn

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M-28

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Category: Cultivated Plants. Grains.

bs Jour: RZhBi:1., H 11, 1958, No 48871

(first half of May) in the non-chernozen zone of USSR are quite feasible even if the temperature of the soil at the depth of 8 cm is below 10c. Along with this, it is necessary that the section be well treated with organic fertilizers and that it be sheltered from the north and northeastern winds. In early string, it is recommended that the seeds be treated with granosan (ethylmercurechloride) and hexachlorane, and not sown deeply. The highest yield of the green mass (together with the cobs) was 540 centners/he was obtained from Sterling variety in 1955 The greatest yield of cobs - 37 1 centners/in was obtained from Moskovsky, Populynt-

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Country: USSR

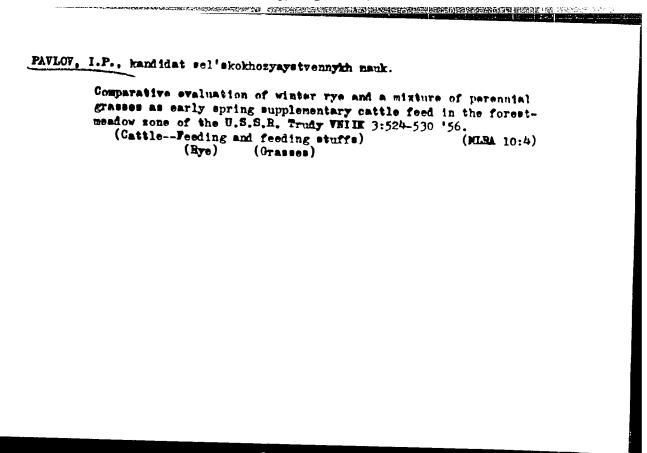
Category: Cultivated Plants Grains.

Abs Jour: RZhBiol., N. 1958, No 48871

siya. June c rm sowings are expedient for green feed and for ensilings. Under the condition of the non-chemiczen belt, the corm varieties of intermediate and late maturity produce the highest yield of feed substances from one hectare at the end of September, and a much lower yield if harvesting takes place before September 20. -- G.N. Chemiov

Card : 3/3

M-29



PAVLOY, I.P., kandidat sel'skokhozyaystvennykh nauk.

Increasing the mineral content of annual and perennial forage grasses. Trudy VNIK 3:531-537 '56. (MUNA 10:4) (Grasses) (Minerals in plants) (Feeding and feeding stuffs)

USSR/Soil Science. Mineral Fertilizers.

I-5

Abs Jour: Referat Zh-Biol., No 6, 25 March, 1957, 22511

Author : Pavlov, I.P. Inst . --- ... .

MALLEN

Title : The Effect of Mineral Fertilizers on Fodder Quality of

Annual Grasses.

Orig Pub: Tr. Vses. n.-i. in-t kormleniya s.-kh. zhivotnikh, 1956, 3,

Abstract: The All-Union Institute of fodder for farm animals conducted a number of field tests to study the effect of mineral fertilizers on the yield of annual grasses and on the content of nutrient substances in several grass mixtures of votch-oats,

vetchling-oats, peliuska-oats and winter rye for green fodder on its experimental farm and in the imeni Chkalov collective farm of Podolsk rayon in the Moscow oblast'. The experimental plan: control (without fertilizer); P 60 kg/hectare; PK 60 kg/

Card : 1/2

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I-5

USSR/Soil Science. Mineral Fertilizers.

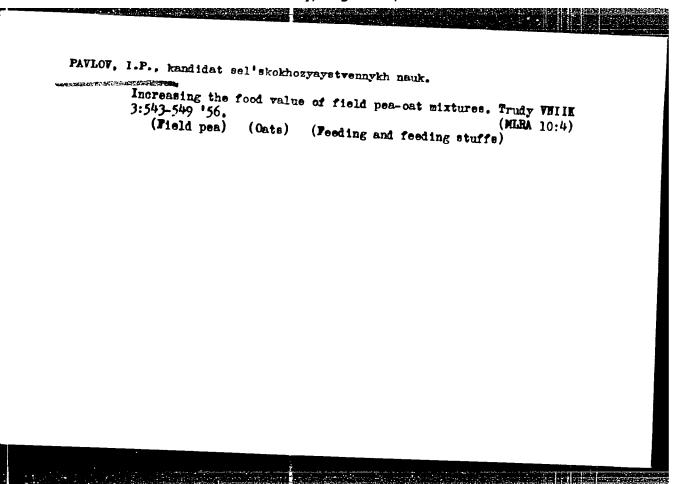
Abs Jour: Referat Zh-Biol., No 6, 25 March, 1957, 22511

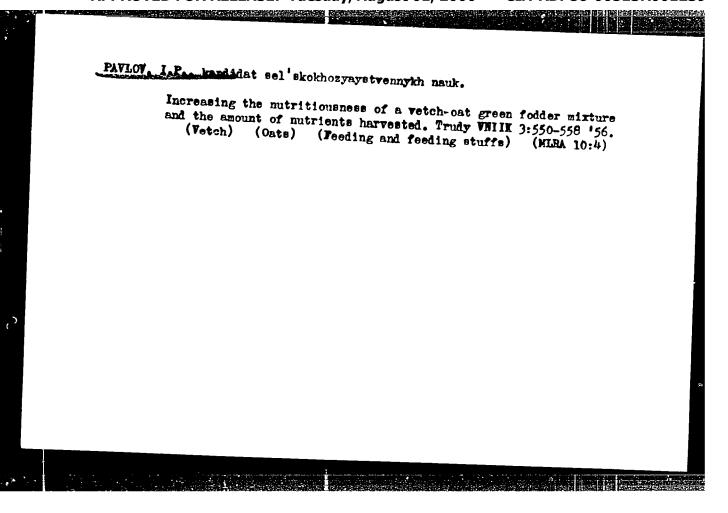
hectare; NPK 60 kg/hectare. It was established that of all the tested mixtures, only the complete mineral fertilizers yield a considerable crop increase (up to 63%) and increase their protein content. P and K without nitrogenous fertilizers show no effect or a very insignificant one on increasing grass productivity.

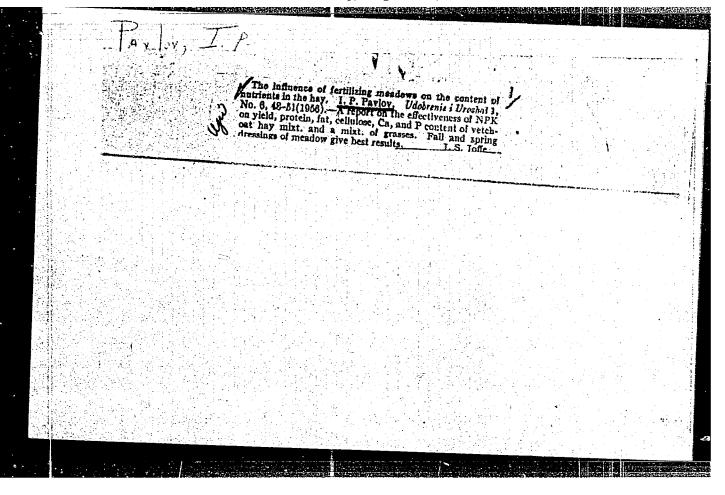
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USSR / Cultivated Plants. Fodders.

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M-4

Abs Jour: Ref Zhur-Biol., No 6, 1958, 25095

: Pavlov, I. P. Inst

: The All-Union Institute for Feeding Agricultural

Title : The Effect of Corn on the Subsequent Vetch-Oats

Orig Pub: Kukuruza, 1957, No 4, 37-39

Abstract: The All-Union Institute for Agricultural Livestock compared in 1955 the effect of corn and perennial

meadow grass mixtures in the second year of use. The vetch-ats mixture's green stuff yield totaled 195.2 after the corn, and 148 centners per ha. after meadow grasses. -- B. K. Flerov

Card 1/1

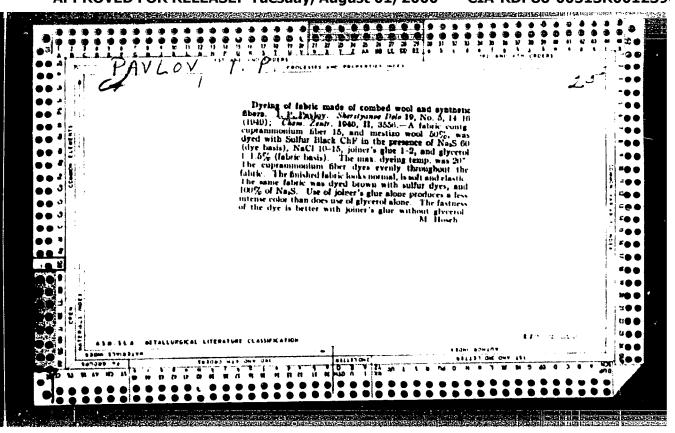
## PAVLOV, I.P., kand. sel'skokhozyaystvennykh nauk

Increasing the amount of protein and other nutritive substances in m mixed perenniel grasses by selecting grass mixture components and by mowing at the optimal time. Dokl. Akad. sel'khoz. 23 no.3:11-16 158.

l. Vsesoyuznyy nauchno-issledovatel'skiy institut zhivotnovodstva. Predstavlena akademikom I.V. Larinym. (Grasses)

VARTANOV, S.Kh.; FAVLOV, 1.5., MERGEYEV, A.J.

Mobile rig for drilling wells in frozen ground. Gaz. prom. 10 nc.9:57 "65. (MIRA 18:11)



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26628 (Peredovaya). Stomatologiya, 1949, No. 3, s. 3-5, s. Portr.

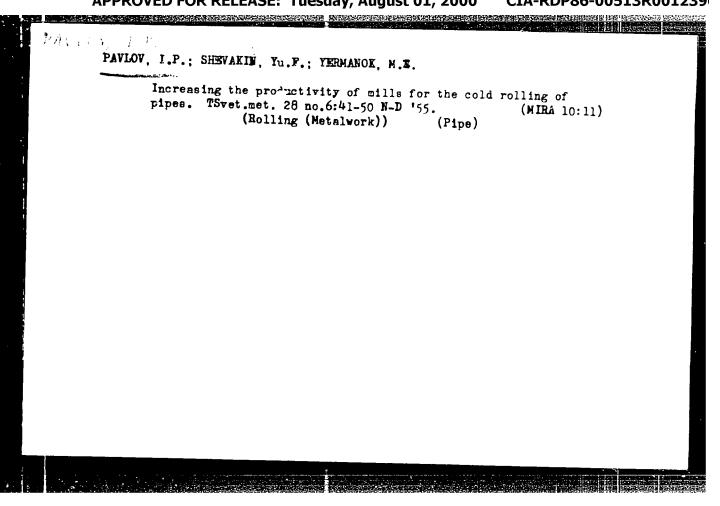
30: LETOPIS' NO. 35, 1949
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PAVICY, I. P. -- "Silov F-Openis of Classic Groupe Over Simple Fields of Characteristic R. " Sub 2s Arm 12, Loccon Clast Personated Inc. (Dissertation for the Degree of Cardidates in Physiconsthermical Sciences).

St: Vechernaya Poshva January-December 1912
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PAVLOV, I. P.: "Immediate and delayed results of the overetimal treatment of votions with heavy penic estempolitis." Second Miscow State Ledders into imensive V. Statement Miscow, 1877. (Discontation for Befree of Canadista in Perical Science).

So: Knizhnava letoris!, N. 23, 1847.



PAVLOV, Ivan Pavlovich; MORDVINTSEV, P.V.

[Guide to practical work in the organization of socialist agricultural enterprises] Rukovodstvo k prakticheskim zanistiiam po organizatsii sotsialisticheskikh sel'skokhoziaistvennykh predpriiatii. Moskva, Sel'khozgiz, 1959. 462 p. (MIRA 13:11) (Parm management)

PAVLOV, I.P.; HELEGKOVA, V.G.

Preparation of activated silicate. Bum.prom. 35 no.10:20-21 0 '60. (MIRA 13:10)

1. Vtoraya bumazhnaya fabrika Memanskogo kombinata.
(Meman—Paper) (Silicate)

PAVLOY, I.P. [Paulau, I.P.], ingh.

How to clean water closets. Rab.i sial. 36 no.5:24 My 160.

(Water closets)

(Water closets)

# \_\_\_PAVLOV, I.P., kand.med.nauk

Immediate and late results of operative treatment of patients suffering from hematogenic osteomyelitis of the long tubular bones. Nauch, trudy Chetv. Mosk, gor.klin.bol?. no.1:196-202 %1.

(MIRA 16:2)

1. Iz kafedry obshchey khirurgii pediatricheskogo fakul'teta (zav. - prof. G.P. Zaytsev) 2-go Moskovskogo gosudarstvemnogo meditsinskogo instituta imeni N.I. Pirogova, na baze Moskovskoy gorodskoy klinicheskoy bol'nitsy No.4 (glavnyy vrach G.F. Papko).

(CSTECMYELITIS) (BONES.—SURGERY)

#### PAVIOV, I.P., kand.med.nauk

Thrombosis and embolism of the pulmonary artery, according to data from pathologico-anatomical studies. Sov.med. 26 no.10: 130-133 0 '62. (MIRA 15:12)

1. Iz kliniki obshchey khirurgii (zav. - zasluzhennyy deyatel' nauki prof. G.P.Zaytsev) pediatricheskogo fakul'teta II Moskovskogo meditsinskogo instituta imeni N.I.Pirogova i 4-y Gorodskoy klinicheskoy bol'nitsy (glavnyy vrach G.F.Papko; prozektor - prof. Ya.L.Rapoport).

(PULMONARY EMBOLISM)